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Our Ref: 502436/24.9/MB/fk

5 April 2024

The Municipal Manager

Mossel Bay Municipality
PO Box 2

MOSSEL BAY

6600

Attention: Mr Lindilizwi Mngxekeza

Dear Sir.

CONSTRUCTION OF INTERNAL CIVIL ENGINEERING SERVICES FOR MOSSEL BAY HOUSING PROJECTS: SINETHEMBA/SEWENDELAAN PHASE 1 LOCATED ON THE REMAINDER OF PTN. 249 OF THE FARM VYF-BRAKKE-FONTEIN No. 220 KWANONQABA, REGISTRATION DIVISION MOSSEL BAY RD

Below please find the Engineering Services Report for Sinethemba, based on the latest preliminary town planning layout as received from Zutari Town Planners, refer to enclosed Drawing no. 113048-0000-DRG-SINE/SEWE, revision 3, dated March 2024.

1. **INTRODUCTION**

1.1 Brief

The Mossel Bay Municipal area has seen a period of rapid growth in recent years which has had the effect that the demand for serviced subsidised erven has dramatically increased.

Mossel Bay Municipality, have submitted a housing subsidy application for 194 serviced housing erven in Mossel Bay as part of the Upgrading of Informal Settlements Programme (UISP) for the greater Mossel Bay Municipal area. The internal reticulation for the proposed residential development will be designed to conform to Municipal standards.

1.2 **General**

The proposed development is adjacent to Sijaji Street, Mzamomhle Street and Nofemela Street within the Kwanonqaba Township. The R102/Louis Fourie Road is towards the North and the N2 Highway towards the North West, when entering from the Mossel Bay CBD, refer to enclosed map: 502436- Upgrading of Informal Settlements. The climate is moderate, with most rainfall occurring mainly during autumn and the mean annual precipitation being in the order of 437mm. The temperature ranges from 18.4°C to 26°C.



The proposed number of developed erven contained is as follows:

Land - Use	No of Erven	Extent (±Ha)	% of Total
Residential Erven	194	1.63	60.15
Road Reserves	-	1.03	38.00
Servitudes	-	0.05	1.85
TOTAL	194	2.71ha	100

2. **BULK WATER SUPPLY SYSTEM**

2.1 **General Description**

The water services infrastructure consists of various raw water sources including the Wolwedans Dam, Klipheuwel Dam, Hartebees Kuil Dam and Ernst Robertson Dam as well as boreholes. Raw water pipelines convey the untreated water to a total of seven water purification plants situated throughout the municipal area. From the various water purification plants, as well as a desalination plant, the treated water is pumped via 30 pump stations into 55 reservoirs.

The total design capacity for the seven water purification plants, as well as the desalination plant, is 72.30 M ℓ per day. The average daily volume of water purified, during the 2015/2016 financial was 20.64 M ℓ per day. The water usage increased to 27.12 M ℓ per day during December 2015. This means that there is between 45.18 M ℓ and 51.66 M ℓ per day spare capacity available.

2.2. Proposed Water Demand for Housing Project

Our calculations are based on the "Guidelines for Human Settlement Planning and Design".

Existing network capacity in the vicinity of the site is subject to the confirmation by Mossel Bay Municipality. GLS Consulting (GLS) were appointed by Mossel Bay Municipality to draw up the Water Master Plan for the Municipal area and to determine the effect of any form of developments in the Municipal area on the Water Master Plan. If required, this and other reports will be submitted to GLS in order to determine whether the existing water network system has sufficient capacity to accommodate the proposed housing development.

According to Table 8.14: Water Demand from ""Guidelines for Human Settlement Planning and Design", the following calculation was done to determine the Annual Average Daily Demand (ADDD) for the various Land Uses: ²

The proposed number of developed erven contained is as follows:

Description	Calculations	Annual Average Daily Demand (AADD)
Residential erven	194 erven x 600ℓ/erf/day	116 400 ℓ/day
Roads	-	0 ℓ/day
	TOTAL AADD	116 400 ℓ/day

This equates to 117 equivalent erven and from the design codes, we expect to design for a peak factor of 7.

Peak Domestic Demand = $116 400 \ell/d \times 7$

= 814 800 ℓ/d

 $= 9.43 \, \ell/s$





Fireflow:

Such a development would fall into a low risk-group 1 category and as such, the following would apply:

- 900 l/min
- 2 hour design fire flow

With the supply spread over a wide area, according to the GLS Water Master Plan the existing reservoirs have sufficient storage capacity and capacity for fire flow conditions to accommodate this particular development.

If required, GLS will be furnished with this and other reports in order to determine whether the existing water storage system has sufficient capacity to accommodate the proposed housing development. According to the Water Master Plan for the Municipal area, sufficient capacity exists at the Water Treatment Plants.

A water reticulation system exists within the adjacent neighbourhoods to which the proposed development will connect (see GLS Figure MBW 2.2b). A system of reservoirs, water pump stations and water mains deliver potable water to developed areas.

2.3 **Proposed Services**

No upgrades to the existing water reticulation system are envisaged in order to accommodate this development, but if required, this and other reports will be submitted to GLS in order to determine whether the existing water network system has sufficient capacity to accommodate the proposed housing development.

As per GLS, Figure MBW 2.1b, water reticulation as well as a potable water pumpstation exists within the proposed construction area. All existing services will either be rerouted or accommodated within the proposed development area.

3. **BULK SEWAGE SYSTEM**

3.1 Wastewater Treatment Works

From the point of origin, all waterborne sewage is conveyed through approximately 510 km gravity sewer pipelines to 73 sewer pump stations situated throughout the municipal area. From the pump stations the sewage is pumped through approximately 40 km of rising main pipelines to a total of seven wastewater treatment plants situated throughout the municipal area. The total design capacity for the seven wastewater treatment plants is 22.54 Ml per day. The current combined average daily inflow for the seven wastewater treatment plants is 10.72 Ml per day.

Wastewater generated from the proposed development will gravitate into the existing system and conveyed by means of gravity sewer lines as well as pumped through rising mains to the Hartenbos Regional Wastewater Treatment Works, where it will be treated.

According to the Sewer Master Plan for the Municipal area, sufficient capacity exists at the Sewage Treatment Plants.

3.2 Wastewater Reticulation System

A normal gravity wastewater reticulation system exists within the adjacent neighbourhoods to which the proposed development will drain (see GLS Figure MBS 2.1b). A system of gravity sewer mainlines, wastewater pump stations and rising mains delivers the accumulated wastewater to the Mossel Bay wastewater treatment works.

3.3 Wastewater Flow Demand

Our calculations are based on the "Guidelines for Human Settlement Planning and Design".

3.3.1 According to the guidelines, the expected average daily wastewater flow per dwelling for the three income groups is as follows:

Income group	Low	Medium	High
Litres per dwelling	500	750	1000
Average persons per dwelling	7	6	5

The proposed area in Phase 1 to be serviced is as follows:

AREA	INCOME GROUP	NO OF ERVEN
Sinethemba	Low	194 erven

Based on the above, the Average Dry Weather Flow (ADWF) for the residential erven would therefore be:

Q = 194×500 Q = $97000 \ell/d$ = $97 k\ell/d$ ADWF = $0.097 M\ell/d$

- 3.3.2 The use of the land is solely for the residential purposes. There will be no other land uses taken into account.
- 3.3.3 The number of persons is:

194 x 7

= 1358 persons

This equates to a peak factor of 2.6.

This would lead to an expected Peak Dry Weather Flow (PDWF) as follows:

Q = $(97000) \times 2.6$ = $252\ 200\ \ell/d$ = $0.252\ M\ell/d$ PDWF = $2.92\ \ell/s$

If an infiltration rate of 15% is used for the ingress of stormwater into the system, the Peak Wet Weather Flow (PWWF) is calculated as follows:

Q = 252 200 x 1.15 = 290 030l/d = 0.29 Ml/d PWWF = 3.36 l/s

3.4 Proposed Services

No upgrades to the existing sewage reticulation system are envisaged in order to accommodate this development, but if required, this and other reports will be submitted to GLS in order to determine whether the existing sewage network system has sufficient capacity to accommodate the proposed housing development.

4. **STORMWATER**

No bulk stormwater systems are required as the stormwater will be dispersed via a number of stormwater outlets into the existing natural watercourse. Accumulated





stormwater will be dispersed by means of energy dissipating structures to minimize the effect of peak runoff downstream.

Currently, stormwater reticulation may exist within the proposed construction area. This is subjected to confirmation during the detailed design phase. All existing services will either be rerouted or accommodated with the future development area.

5. ACCESS ROADS

Access to the proposed development area will be provided from the North-West from Thembelihle Ave, North from Nofemela St or North from Sijaji St. No upgrades to the existing road infrastructure is required. The points/roads allocated where access will be available to the area will need to be upgraded, stabilized or filled with material to give proper movement of vehicles in and out of the site.

6. **SOLID WASTE**

Refuse removal will be dealt with once a week as applicable to all the current residential areas in the Mossel Bay Municipal area.

Solid waste is based on an estimated 3.5 kg/person/day.

Therefore: (194 units x 7 people per unit x 3.5 kg/day)

= 4753 kg/day = 4.753 tons/day

Volume = 4.753 t/d x 0.75

 $= 3.57 \text{ m}^3/\text{d}$

 $= 107.10 \text{ m}^3/\text{month}$

Based on preliminary discussions with Mossel Bay Municipality the existing solid waste site will be able to accommodate the additional solid waste generated by the development. An existing solid waste processing and transfer site is located within, the development area will be accommodated within the final development layout.

7. **FLOODLINES**

This housing project is not affected by a floodline within the proposed development area.

8. EXTRAORDINARY DEVELOPMENT CONDITIONS AND LAND REHABILITATION

The general terrain and the underlying geology of these sites appear to be suitable for housing development. Some of the sites that are adjacent to natural drainage lines are quite steep and some terracing may be necessary. Most of these sites are presently occupied by informal structures and there is evidence of some disturbance to the natural ground level due to uncontrolled fill and/or rubbish dumping, but this is not considered severe and can probably be cleared off the sites. No other severely problematic soils are expected and conventional engineering is envisaged.

Shallow hard rock is expected within 1.5m in some areas in Kwanonqaba and the depth to the rock is likely to vary widely. Excavations into rock are classified as "Hard" in terms of SABS 1200D. The in situ soils are unsuitable for use as pipe bedding or blanket due to the presence of coarse soil or clumps of clay that does not meet grading or compactibility requirements. Pipe bedding and blanket materials will have to be imported from local quarries. The in situ soil may be suitable for use as backfilling over pipe blanket, but this will have to be confirmed. With respect to the construction of internal access roads, it is



likely that the in situ subgrade is poor on all sites and an imported selected subgrade layer is envisaged for roads. The installation of services will be particularly challenging on steep slopes.

These conditions have certain implications for the installation of services and thus the motivation is based on the necessity for:

- a) Removing and disposal of the uncontrolled fill material from site;
- b) Importing of backfill material for filling of disturbed ground areas;
- c) Stormwater interventions on steep slopes to prevent erosion;
- d) Creation of Housing Platforms on steep slopes;
- e) Construction of Retaining Walls for housing platforms; and
- f) Importation of selected layers for road construction.

Estimates regarding the additional cost over and above the housing subsidy amount can be submitted once detail designs have been completed and revised as soon as formal tenders received.

9. **INTERNAL SERVICES**

The proposed internal civil services are indicated on Drawing No's 502436-SINE-DRG-CC-0001. Below finds a brief description of the services to be provided for the area.

9.1. Sewage

1265m of 160mm dia PVC-u heavy duty sewer pipe

87 No. Manholes

110mm dia PVC-u light duty house connections with end cap for 194 erven.

9.2 Water

17m of 75mm dia PVC-u Class 12 water pipe

220m of 90mm dia PVC-u Class 12 water pipe

1050m of 110mm dia PVC-u Class 12 water pipe

14 No. Gate valves

4 No. Fire hydrants

20mm dia HDPE Class 12 water house connections for 194 erven

9.3 Roads

5300m², paving roads. Road widths vary from 3.5m - 5.5m wide with Barrier/Mountable kerb and channels on the lower side of the roadway and concrete channels at intersections.

9.4 Stormwater

2010m of Barrier/Mountable kerb and channel

520m of 450mm dia concrete stormwater pipe

13 No. Stormwater Catchpits





2 No. Stormwater Manholes

2 No. Brick headwalls

10. STANDARD OF ENGINEERING SERVICES TO BE PROVIDED

Levels of services are as follows:

10.1 **Sewer**

- Pipe diameter: 160mm dia solid wall for main lines and 110mm solid wall for house connections. UPVC Class 34 or Ultracor Class 400 Heavy Duty (400 kPa).
- Precast concrete rings to be used for manholes.
- Erf connection ends 1m into the erf with a rodding eye.

10.2 **Water**

- Pipe diameter of 75 160 mm dia MPVC Class 9/12 pipes depending on residual pressure.
- Each erf will be serviced with a 20mm diameter connection and an Elster Kent/Honeywell plastic water meter in a plastic meter box or similar approved meter by the Technical Services Directorate.
- Provision is made for fire hydrants according to "Red Book" guidelines.
- All fire hydrants shall be 65mm dia (internal)
- All fire hydrant outlet shall be of bayonet coupling type.
- All valves shall be AVK type valves left hand/closing or similar approved.

10.3 Roads and stormwater

- The road width will be 4.5m in 8 and 10m reserves and 5.5m in 13 and 16m reserves.
- All road surfaces will be either Cape seal or paved surface.
- Sub-base and base materials will be imported.
- Sub-surface drainage, where applicable, will be installed.
- The underground piped stormwater drainage system will be minimum 375mm diameter.
- Barrier kerbs will be installed around bellmouths. Bellmouth's radius minimum 10m
- All stormwater drains will be provided with a sand trap of at least 300mm.

10.4 **Design Criteria and Standards**

10.4.1 Design criteria

The following documents will serve as a base for the detail design criteria and standards:

- Guidelines for Human Settlement Planning and Design ("Red Book"); and
- City of Cape Town Management of Urban Stormwater Impacts Policy Version 1.1, 2009.





10.4.2 Construction specifications

All materials and workmanship shall comply with the specifications as set out in the South African National Standards for Civil Engineering (SANS).

10.4.3 Roads

The road system forms an integral part of the local area plan.

10.4.3.1 Design Criteria

The design criterion for roads is as follows:

- Road reserve widths are 16m, 13m, 10m and 8m.
- Design life of the roads is 20 years.
- Sub-grade CBR 15 to 20.
- Sub-base CBR 45min. (processed crushed stone)
- Base course CBR 80min. (processed crushed stone)
- Surfacing minimum gravel wearing course on all roads.
 - alternatives Cape seal or paving
- Minimum road grade 0.45 %
- Minimum road crossfall 2 %

10.4.4 Stormwater

The storm water system forms an integral part of the road and urban planning layout. The system rests on three legs, the minor system, the major system and an emergency system. The minor storms are catered for in the pipe system while the major storms are routed through a linked system of roads and public open spaces using attenuation techniques. The emergency system recognizes failure of the minor and major system by storms greater than provided for in major system or in the event of malfunction of the minor system by providing continuous overland flow routes to minimize flooding of residential areas.

10.4.4.1 Minimum design criteria for storm water system

The data to be used for the design of the system is as follows:

- Minor system : 2-year return period conveyed in an underground pipe system.
 Preferably the overland flow shall not exceed 200m.
- Major system: 50-year return period. The difference between the 2 year and 50 year to be conveyed in the road prism with depth not exceeding 150mm within the road reserve width.
- The minimum gradients for pipelines are designed to give a minimum velocity of 0.7m per second with the pipe flowing full.
- The maximum velocity used is 3.5m per second.
- Major storm water overflows are to be provided to convey the excess storm water from the streets into designated public open spaces.
- Storm water flow velocities in roadways will be kept as low as possible and related to the surface finish to prevent scour and erosion.
- Roads are to be graded to ensure free and continuous flow to the main storm water system and to prevent local ponds at intersections.

10.4.4.2 Pipelines

- Storm water pipes are generally 50D, 75D or 100D as required by the loading and installation conditions.
- Pipes are generally laid on Class C bed.
- The minimum cover on pipes is 0.80m.





• The minimum pipe diameter is 375mm for longitudinal runs and catch pit connections.

10.4.6 <u>Sewers</u>

The sewer drainage system forms an integral part of the sewage system. The drainage for the site is in different directions due to the topography of the site.

10.4.6.1 Minimum design criteria

 A conventional waterborne sewerage system is provided with single connections to individual erven. The main sewer line will be constructed within roads reserves or midblock sewers on the site topography depending.

• Design parameters : Average daily flow - 500l / erf / day

: Peak factor – Harmon formula

: Extraneous flow - 15 %

: Minimum velocity – 0.7m per second

Minimum cover to pipes : 0.80m

Minimum pipe size : 110mm diameter for house connections

: 160mm diameter for sewer mains

Minimum gradients : 110mm diameter house connection 1:60

: main lines at 80% capacity as follows:

Dwelling units	Grade
Less than 6	1:80
6 to 10	1:100
11 to 80	1:120
81 to 110	1:150
111 to 130	1:180

- House connection depth shall generally be 1.0m but at least be able to drain 80% of an erf.
- Maximum manhole spacing of 80m.

10.4.6.2 Pipelines

- Pipeline material for pipe sizes up to 160mm diameter :
 - uPVC Class 34 Ultracor Class 400 400 Heavy Duty (400 kPa) complying with SABS
- Pipes are generally laid on Class C bedding.

10.4.6.3 *Manholes*

- Dolomite aggregate and low alkali sulphate resistant cement to SABS 471 shall be used for all concrete, mortar or screed.
- Manhole cover to be central over main pipe on downstream side.
- Manhole covers and frames to be Concrete.

10.4.7 Water

The water reticulation network forms an integral part of the water distribution system.



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10,4.7.1 Minimum design criteria

The design criteria generally as per the "Red Book" guidelines and specifically as follows:

- An average domestic consumption of 600l per day per erf.
- Peak factors for the development will be calculated in accordance with Figure 9.9 of the "Red Book".
- Minimum pressures for the network are calculated for the fire flows of 30l per second and peak demand at the point of lowest pressure under peak flow conditions.
- Valves to be placed such that a maximum of 4 valves need to be closed to isolate a section of pipeline.
- Valves to be spaced so that the length of main included in an isolated section does not exceed 600m.
- All valves to be installed at T-pieces where applicable and not within the road surface.
- Minimum cover to pipe to be 0.8m.

10.4.7.2 Pipeline materials

- Network uPVC Class 9/12, dia 75 160mm complying to SABS 966
- Erf connections HDPE Class 12, JASWIC

We trust that we have provided sufficient information for your purposes and look forward to hearing from you shortly. Please do not hesitate to contact us if you should require any further information.

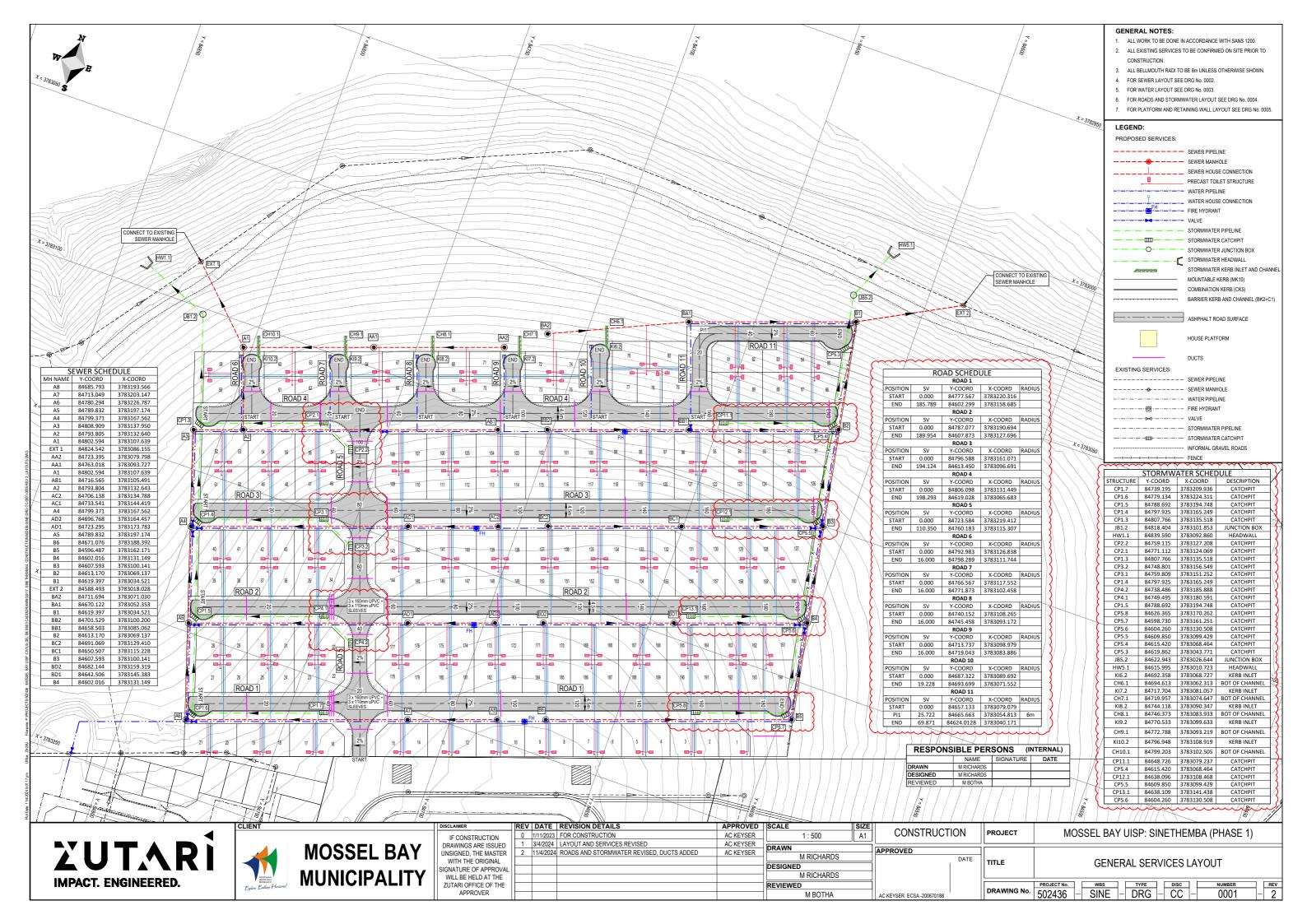
Yours faithfully

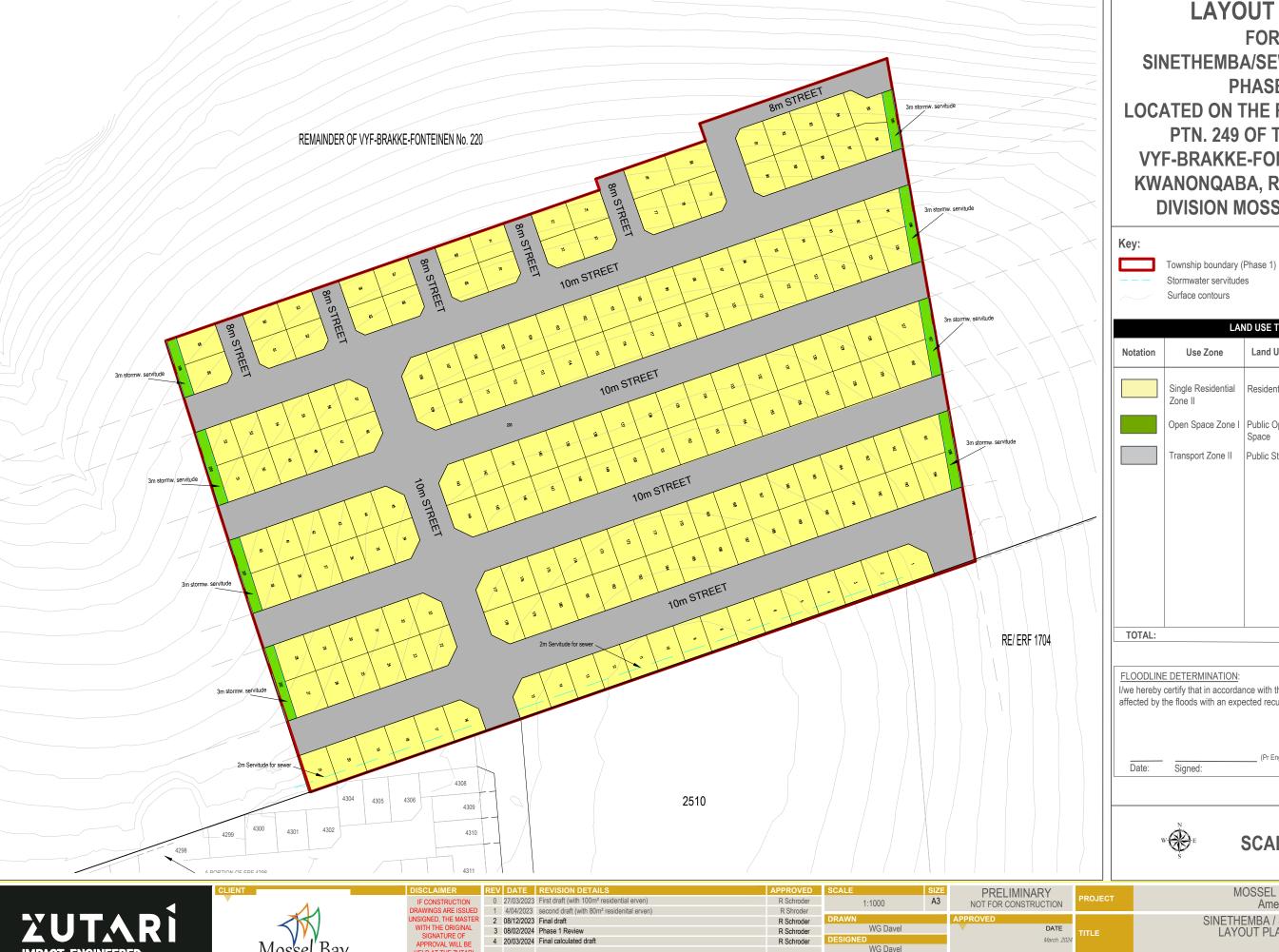
M BOTHA Pr Tech Eng Technical Specialist pp Zutari AC Keyser Pr Tech Eng Office Manager pp Zutari

Enc: Drawing No. 113048-0000-DRG-SINE/SEWE

Map : 502436 – upgrading of informal settlements

GLS Figure MBS 2.1b GLS Figure MBW 2.2b





LAYOUT PLAN FOR SINETHEMBA/SEWENDELAAN PHASE 1 LOCATED ON THE REMAINDER OF PTN. 249 OF THE FARM VYF-BRAKKE-FONTEIN No. 220 KWANONQABA, REGISTRATION **DIVISION MOSSEL BAY RD**

LAND USE TABLE					
Notation	Use Zone	Land Use	Erf nos	Number of erven	Area (ha)
	Single Residential Zone II	Residential	1-194	194	1.6230ha
	Open Space Zone I	Public Open Space	195-202	8	0.0480ha
	Transport Zone II	Public Street	203	1	1.0259ha
TOTAL:				203	2.6971ha

I/we hereby certify that in accordance with the Water Act, 1998, the area is not affected by the floods with an expected recurrence interval of 1:100 years.

(Pr Eng) Registr No.

SCALE: 1:1000



R Schroder

MOSSEL BAY UISP Amended SINETHEMBA / SEWENDELAAN LAYOUT PLAN - PHASE 1

 DRAWING No.
 PROJECT No.
 WBS
 TYPE
 DISC
 NUMBER
 REV

 3
 SIN / SEWE 3

